

Under Voltage Load Shedding Using Trajectory Sensitivity Analysis Considering Dynamic Loads

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Abstract Under voltage load shedding is a proficient counter-measure action against voltage instability/collapse. UVLS procedure is an effective means to maintain voltage stability of a power system when the system's voltage is just about to collapse following some disturbances. This paper proposes an advanced under voltage load shedding based on trajectory sensitivity analysis for voltage stability enhancement. Trajectory sensitivity analysis is a technique based on linearizing a system surrounding a certain trajectory and employs time domain simulations. This technique computes the sensitivity of the dynamics relating to the constraints. Trajectory sensitivities between bus voltages are calculated by using hybrid system's trajectory sensitivities to obtain sufficient amount for load shedding. Furthermore, trajectory sensitivity index at all buses is calculated to select the most appropriate location of load shedding. Dynamic simulations are performed with the 14 bus RTS IEEE as case study.

Keywords Under Voltage Load Shedding, Dynamic Load, Trajectory Sensitivity Analysis

1. Introduction

As the power system become more complex and heavily stressed, voltage stability problems also become more severe. During planning and operation of power system, voltage problems now have become a great concern, because of significant amount of failures which is believed that have been caused by voltage instability. Since 1920s, power system stability has been identified as a crucial prerequisite for a safe and reliable operation of electricity power system [1]. The instability of the power system has instigated disturbance expansion [2]. Specifically, transient voltage instability, which in the recent years steadily ascends following occurrence of line outage or short circuit. The importance of maintaining electric power system stability and reliability has motivated the developing of new methods to mitigate the system instability. Voltage instability can bring the whole network system to significant voltage drop

condition, therefore alleviation action is required. One of the mitigation action for voltage instability as discussed in [3, 4] is under voltage load shedding (UVLS) which is an economical way of alleviating system collapse where small load cutback between 5% and 10% can maintain the stability of the system. UVLS has been employed for a long time as the last remedy to evade major power system breakdown which is triggered by under voltage relays. UVLS is occupied by instantaneously shedding a certain amount of load to prevent voltage drop and to maintain the system equilibrium. Research and experience have provided evidence that UVLS is a powerful counter-measure action to preclude voltage instability.

Two core issues of UVLS are determining proper amount of load shedding and finding appropriate location for load shedding. Nonetheless, these problems are intricate in practical operation of UVLS. UVLS must shed adequate amount of loads to recover to a stable condition, yet not overly sensitive. Hence this paper aims to provide an advanced design of under voltage load shedding employing trajectory sensitivities methodology. Trajectory sensitivities between bus voltages are calculated by using hybrid system's trajectory sensitivities to obtain sufficient amount for load shedding. Then trajectory sensitivity index at all buses is calculated to select the most appropriate location of load shedding. The proposed methodology is implemented on the 14-bus IEEE Reliability Test System. Dynamic simulation is performed to validate the robustness of the proposed method.

This paper is organized as follow. Section 2 explains power system under voltage load shedding. Section 3 describes about dynamic load modeling. The proposed method: trajectory sensitivity analysis based UVLS design is presented in Section 4. Section 5 gives the results and analysis and Section 6 concludes the main findings of the research. Findings of this research are expected to provide a better UVLS setting to confront the probability of voltage collapse incident.

2. Power System under Voltage Load Shedding

UVLS is an economical option to maintain voltage stability while waiting for completion of new generation or transmission lines project [5]. Many utilities around the world have applied UVLS schemes. Reference [6] provides existing UVLS applications in some utilities with their specific setting. The philosophy of UVLS is that whenever the system is disrupted then lead to voltage drop condition below a certain pre-selected level for a certain pre-determined time period, then selected loads should be removed [7]. It is expected that the system voltage will retrieve to its normal limit by cutting off some loads. The objective of a UVLS is to reinstate the balance power within the system, to avert voltage collapse and to manage the voltage problems reside within a local area rather than permitting it to spread out to other areas [8]. The design of a load shedding should be “robust”. UVLS must cover enough loads as well as not overly sensitive. Therefore, there are some considerations to ensure efficient load shedding [7, 9]:

- *Determination of amount of load to be shed:* Shedding adequate amount of load is imperative in order to ensure UVLS can mitigate the menace of voltage instability. Shedding insufficient amount of the necessitated load will not be effective in arresting voltage collapse, on the other hand, shedding more load than required may lead to an over frequency circumstances.
- *Selection of location of load to be shed:* Study in [10] shows that shedding load in the correct location can arrest voltage instability. However, shedding the same amount of load in different location gives different result and may not be effective to improve the system stability.
- *Determination of timing and time steps of load shedding:* Load shedding is executed in steps in order to preclude over shedding condition. The minimum time delay before a UVLS is triggered should be sufficient in preventing voltage collapse as well as avoiding unnecessary tripping during transient time where load shedding is unnecessary.

3. Dynamic Load Modeling

Load modeling is one of the most significant components in dynamic voltage stability simulation including under voltage load shedding. In this work, the load at each bus is represented as composite load which is a combination of static load and dynamic load. Figure 1 shows the equivalent circuit of a composite load model, where Z , I , P are constant impedance, constant current and constant power, respectively; X_m is magnetizing reactance; X_s is stator leakage reactance; X_r rotor leakage resistance; R_s is stator resistance; R_r is rotor resistance; and s is induction motor slip.

Dynamic load model is important for UVLS design [11], because induction motors will decelerate substantially if their terminal voltage falls as a result of short circuits [12].

The generic load dynamic models are [13-16]

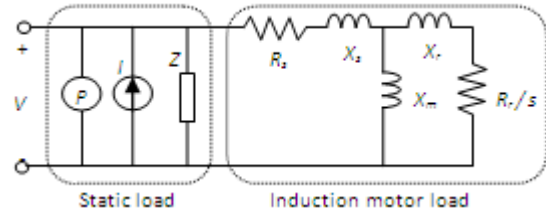


Figure 1. Schematic circuit of the composite load model

$$T_p \frac{dP_d}{dt} + V^{\alpha_t} P_d = V^{\alpha_s} P_s(V) + \alpha_t T_p \frac{P_d}{V} \frac{dV}{dt} \quad (1)$$

$$T_q \frac{dQ_d}{dt} + V^{\beta_t} Q_d = V^{\beta_s} Q_s(V) + \beta_t T_q \frac{Q_d}{V} \frac{dV}{dt} \quad (2)$$

Where,

$P_s(V)$ and $Q_s(V)$ steady state load for real and reactive power, respectively, as function of voltage;
 $P_t(V)$ and $Q_t(V)$ transient load for real and reactive power, respectively, as function of voltage;
 P_d and Q_d instantaneous real and reactive power, respectively;
 T_p and T_q time constant for real and reactive power, respectively;
 x_p and x_q load state variable for real and reactive power, respectively;
 α_t , α_s , β_t , β_s , P_1 and Q_1 are constants independent of load busbar voltage V .

4. Trajectory Sensitivities Enhanced UVLS Scheme

4.1. Trajectory Sensitivity Analysis

Trajectory sensitivity analysis is a technique based on linearizing a system surrounding a certain trajectory and employs time domain simulations [17]. This technique computes the sensitivity of the dynamics relating to the constraints [18]. Trajectory sensitivity provides a method of enumerating changes in the system variables in connection with the quick changes of system parameters and initial conditions [19]. The basic methodology of trajectory sensitivity computation of hybrid systems is illustrated in [19] as follow.

The systematical representation for voltage stability analysis of a power system is provided by the following differential-algebraic equation (DAE),

$$\dot{x} = f(x, y; \alpha) \quad (3)$$

$$0 = g(x, y; \alpha) \quad (4)$$

Where x is the vector of dynamic state variables; y is the vector of algebraic state variables such as load bus voltage magnitudes and angles; and α represents system parameters, such as power.

Trajectories of (3) and (4) illustrates the performance of

the dynamic variables x and algebraic variables y , where flows of x and y can be defined, as

$$x(t) = \varphi_x(x_0, t, \alpha) \quad (5)$$

$$y(t) = \varphi_y(y_0, t, \alpha) \quad (6)$$

Sensitivities of the flows φ_x and φ_y to the initial conditions and parameter variations can be acquired by forming the Taylor series expansions of above equations, hence

$$\begin{aligned} \Delta x(t) &= \Delta \varphi_x(x_0, t, \alpha) = \frac{\partial \varphi_x(x_0, t, \alpha)}{\partial \alpha} \Delta \alpha \\ &= \frac{\partial x(t)}{\partial \alpha} \Delta \alpha \cong x_\alpha(t) \Delta \alpha \end{aligned} \quad (7)$$

$$\begin{aligned} \Delta y(t) &= \Delta \varphi_y(y_0, t, \alpha) = \frac{\partial \varphi_y(y_0, t, \alpha)}{\partial \alpha} \Delta \alpha \\ &= \frac{\partial y(t)}{\partial \alpha} \Delta \alpha \cong y_\alpha(t) \Delta \alpha \end{aligned} \quad (8)$$

An approximation based numerical method is used to compute the sensitivities x_α and y_α , consequently,

$$\begin{aligned} x_\alpha &= \frac{\partial x}{\partial \alpha} = \frac{\Delta x}{\Delta \alpha} \\ &\approx \frac{\varphi_x(x_0, t, \alpha + \Delta \alpha) - \varphi_x(x_0, t, \alpha)}{\Delta \alpha} \end{aligned} \quad (9)$$

$$\begin{aligned} y_\alpha &= \frac{\partial y}{\partial \alpha} = \frac{\Delta y}{\Delta \alpha} \\ &\approx \frac{\varphi_y(y_0, t, \alpha + \Delta \alpha) - \varphi_y(y_0, t, \alpha)}{\Delta \alpha} \end{aligned} \quad (10)$$

The trajectory sensitivities from (8) and (10) are revised to meet the purpose of this study. The bus voltage magnitude and load shedding amount are both parameters represented by y and α correspondingly, hence sensitivities of bus voltage variation after load shedding at any specified bus are computed can be defined as

$$\begin{aligned} \Delta V(t) &= \Delta \varphi_V(V_0, t, P) = \frac{\partial \varphi_V(V_0, t, P)}{\partial P} \Delta P \\ &= \frac{\partial V(t)}{\partial P} \Delta P \cong V_P(t) \Delta P \end{aligned} \quad (11)$$

$$\begin{aligned} \varphi V_P &= \frac{\partial V}{\partial P} = \frac{\Delta V}{\Delta P} \\ &\approx \frac{\varphi_V(V_0, t, P + \Delta P) - \varphi_V(V_0, t, P)}{\Delta P} \end{aligned} \quad (12)$$

4.2. Trajectory Sensitivity Factor

In addition, the trajectory sensitivities are performed to find the load shedding location. A trajectory sensitivity factor (TSF) is formulated to assess the contribution of bus j after load shedding to the system voltage stability. The sensitivities calculated are $[\partial V_i / \partial P_j]$, which inform the rate of change in voltage magnitude at bus i with respect to the load shedding amount variation at bus j . The TSF at bus j is computed by shedding active power at bus j by a small value then assessing its impact on voltage magnitudes at all critical buses along time domain. The TSF proposed in this work is

defined as

$$TSI_j = \sum_{i=1}^{n_k} \left[\sum_{t=0}^{t_s} \left[\frac{\partial V_i}{\partial P_j} \right]_{t=t_k} \right] \quad (13)$$

$$\partial P_j = \Delta P_j = P_{shed_j}$$

Where,

P_{shed_j} load shedding amount at bus j

n_k number of critical buses

t_k time instant

t_s number of time instant

The bus with the highest TSF means that this bus has the largest effect on the voltage stability improvement of the critical buses hence will be selected as a candidate bus for location of UVLS. The proposed trajectory sensitivities based UVLS can be explained as follow:

Step 1 Set load shedding amount. In this work, the load shedding amount is set at 5 MW for each iteration.

Step 2 Select an outage.

Step 3 Perform dynamic voltage stability analysis to observe the voltage behavior for all buses.

Step 4 Identify critical zones. This is a zone where buses in have similar pattern of voltage drop.

Step 5 Perform trajectory sensitivity analysis to evaluate the bus voltage trajectory sensitivities.

Step 6 Calculate TSF (13) to assess the contribution of each load bus on improving voltage stability of the buses the critical zones. The bus with the highest TSF has the most influence to improve the system voltage magnitude. The location of load shedding is determined based on the highest TSF value.

Step 7 Load shedding is applied in the selected bus.

Step 8 Perform dynamic voltage stability analysis to evaluate the system performance after load shedding

Step 9 If the system is still unstable, then the network data is updated and go Step 5. This process will be reiterated until the voltage stability constraint is satisfied

Step 10 If the voltage stability requirement has been fulfilled, then write the results and stop the process.

3. Results and Discussion

TSF as in (13) is applied to determine the load shedding amount and location. As mentioned above, the bus with the highest TSF has the biggest effect on the voltage stability. The proposed method is implemented at the IEEE 14 bus Reliability Test System (Figure 2).

The system is assumed to be working on a stressed condition. The system load for this study is 511.36 MW, consisting of 50% static load and 50% dynamic motor load. Prior to designing the UVLS scheme, contingency analysis is performed to choose the critical outage. Based on this analysis, the outage between bus 6 and bus 13 is chosen in this study. For the dynamic simulation, a fault is applied between bus 6 and bus 13, and then the fault is cleared by

removing the transmission line between bus 6 and bus 13. Figure 3 shows the voltage drop after disturbance. There are five critical buses at which the voltage collapses below the stability limit (0.9 pu). They are buses 9, 10, 12, 13 and 14 as shown in Figure 4.

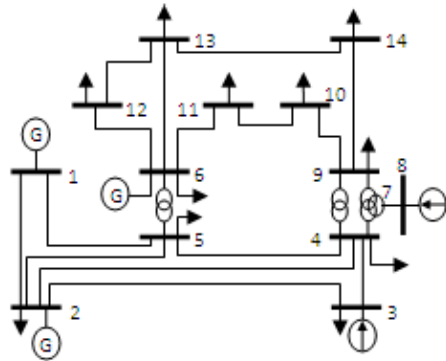


Figure 2. The test system – IEEE 14 Bus Reliability Test System

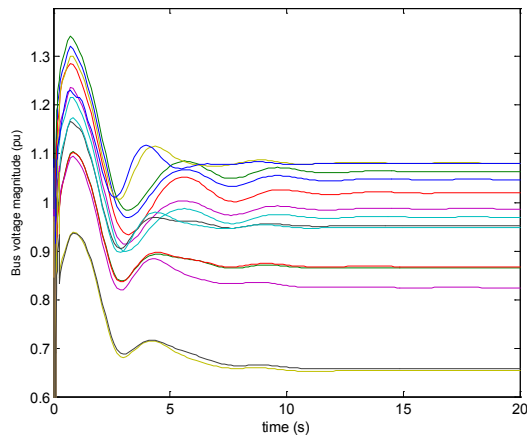


Figure 3. Voltage drop at all buses after outage between bus 6 and bus 13

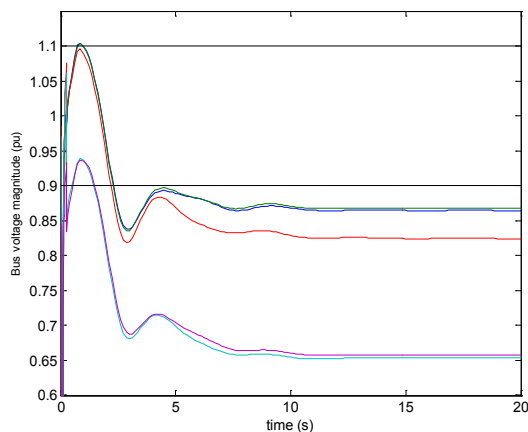


Figure 4. Voltage drop at the critical buses after outage between bus 6 and bus 13

For this simulation, the load shedding amount for each iteration is set at approximately 1% of the total system load. In this case, we round the amount to 5 MW for each step. The trajectory sensitivity analysis is performed to assess the effect of load shedding of 5 MW at each bus in the critical

zone. Figures 5 and 6 illustrate the voltage trajectory sensitivities of critical buses for the first iteration if load shedding is commenced at bus 14 and bus 6, respectively. From both of these figures, it can be concluded that the voltage trajectory sensitivities if load shedding occurs at bus 14 are better than the sensitivities at bus 6. Furthermore, TSF is calculated to provide a distinct indication for load shedding location. In computing the TSF value, we use time interval 0.5 seconds for the period 0 to 20 seconds. Table 1 illustrates the TSF calculation for load shedding at buses 14 and 6.

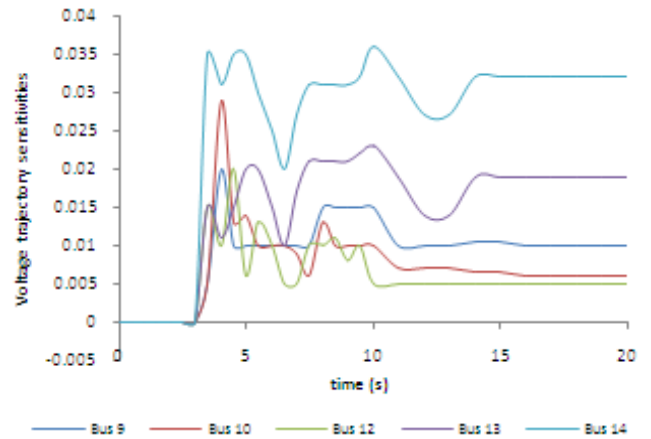


Figure 5. Bus voltage trajectory sensitivities of critical buses if load shedding is 5 MW at bus 14

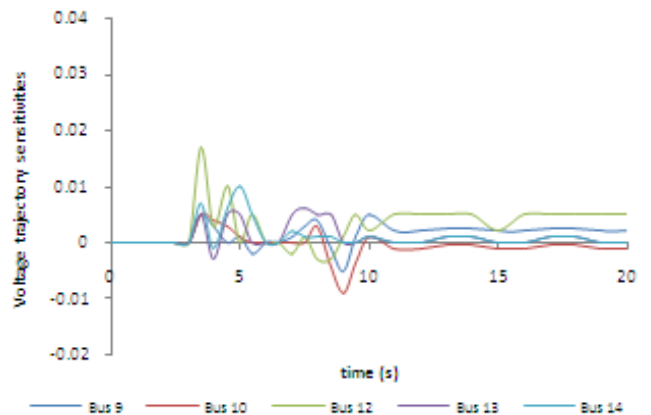


Figure 6. Bus voltage trajectory sensitivities of critical buses if load shedding is 5 MW at bus 6

Figure 7 depicts the TSF value for each load bus at the first iteration. As indicated in the red bar, bus 14 has the highest TSF (1.854). Load shedding of 5 MW is simulated at bus 14 and the system voltage magnitude is re-evaluated. At this stage, the system is still unstable; hence, trajectory sensitivities are performed again to calculate the TSF. For this simulation, this process is repeated six times until the system voltages are stable (above 0.9 pu). The results of the TSF calculation for each iteration and load shedding location based on the highest TSF are presented in Table 2 and Table 3, respectively. Hence, the load shedding locations are bus 14 and bus 13 with a load shedding amount at each bus of 15

MW. The results of the voltage improvement after load shedding of 30 MW at buses 14 and 13 can be seen in Figure 8. It clearly proves that the voltages at all buses improve significantly and that the system stability is recovered.

Table 1. TSF Calculation

$\sum_{t=0}^{t_s} \left[\frac{\partial V_i}{\partial P_j} \right]_{t=t_k}$		
Bus <i>j</i>	14	6
Bus <i>i</i>		
9	0.271	0.037
10	0.223	-0.008
12	0.188	0.083
13	0.432	0.038
14	0.74	0.037
	1.854	0.187

4. Conclusions

This paper proposes a new design of under voltage load shedding for stabilizing the system following disturbance and ensuring the system secure limits are satisfied. The design is based on trajectory sensitivity technique that calculates the sensitivity of the dynamics relating to the constraints and provides a method of enumerating changes in the system variables in connection with the quick changes of system parameters and initial conditions. Trajectory sensitivity is employed to determine the minimum amount of load shedding and sensitivity index is used to verify location of load shedding.

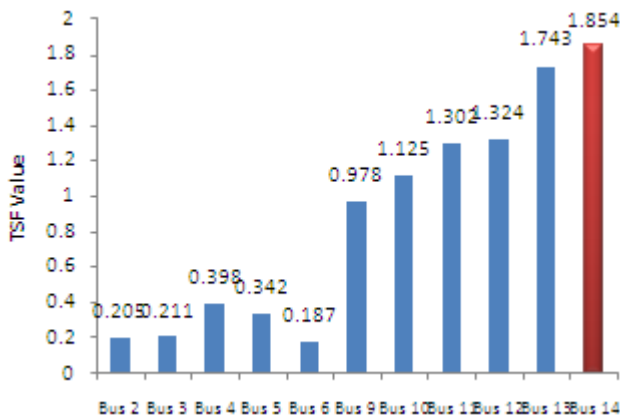


Figure 7. TSF values at first iteration

The IEEE 14-bus Reliability Test System indicates that the trajectory based under voltage load shedding can effectively improve the system voltage behavior performance after outage. This proposed method can offer minimum disruption in load shedding while still ensuring post-fault voltage stability within the limits.

Table 2. TSF values

Iteration	TSF Value					
	I	II	III	IV	V	VI
Bus Number						
2	0.205	0.134	0.110	0.098	0.074	0.026
3	0.211	0.167	0.149	0.106	0.079	0.034
4	0.398	0.302	0.257	0.211	0.086	0.057
5	0.342	0.264	0.216	0.174	0.123	0.089
6	0.187	0.112	0.098	0.077	0.056	0.034
9	0.978	0.849	0.798	0.731	0.674	0.324
10	1.125	1.046	0.987	0.923	0.879	0.585
11	1.302	1.213	1.168	1.092	1.021	0.793
12	1.324	1.265	1.205	1.158	1.115	0.967
13	1.743	1.419	1.367	1.257	1.187	1.076
14	1.854	1.578	1.319	1.296	1.159	1.025

Table 3. Load shedding locations

Iteration	Load Shedding Design	
	Location	Amount (MW)
I	Bus 14	5
II	Bus 14	5
III	Bus 13	5
IV	Bus 14	5
V	Bus 13	5
VI	Bus 13	5

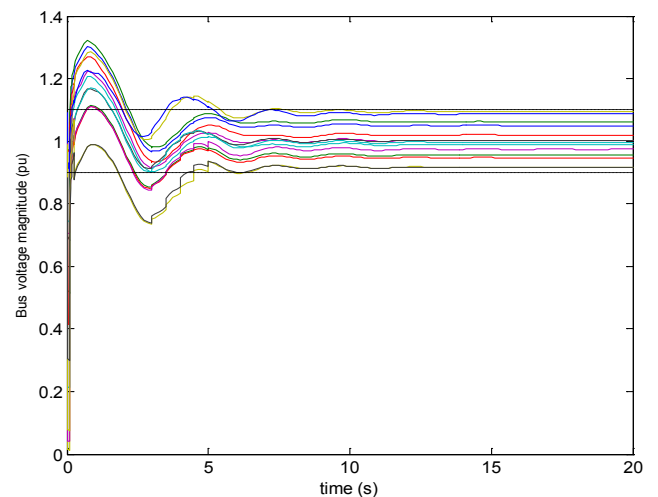


Figure 8. Voltage profile improvement after load shedding

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